



## BU808DFI

### HIGH VOLTAGE FAST-SWITCHING NPN POWER DARLINGTON

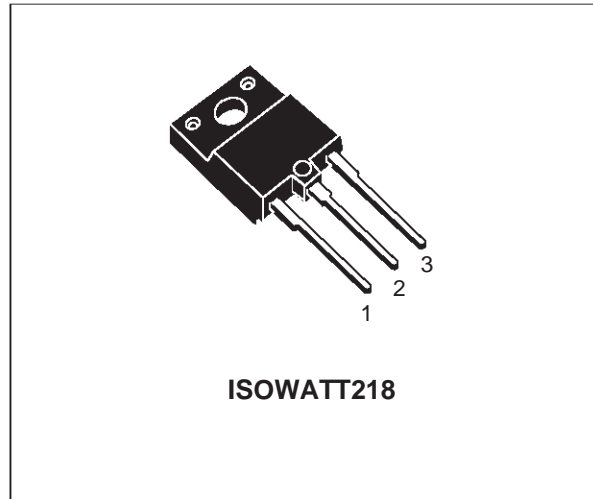
- STMicroelectronics PREFERRED SALESTYPE
- NPN DARLINGTON WITH INTEGRATED ANTIPARALLEL COLLECTOR-EMITTER DIODE
- HIGH VOLTAGE CAPABILITY
- HIGH DC CURRENT GAIN
- U.L. RECOGNISED ISOWATT218 PACKAGE (U.L. FILE # E81734 (N))
- LOW BASE-DRIVE REQUIREMENTS
- COST AND SPACE SAVING.

#### APPLICATIONS

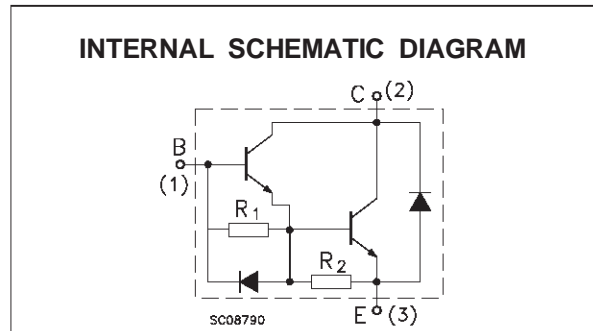
- HORIZONTAL DEFLECTION FOR COLOUR TV

#### DESCRIPTION

The BU808DFI is manufactured using Multiepitaxial Mesa technology for cost-effective high performance.



ISOWATT218



#### ABSOLUTE MAXIMUM RATINGS

Symbol	Parameter	Value	Unit
$V_{CBO}$	Collector-Base Voltage ( $I_E = 0$ )	1400	V
$V_{CEO}$	Collector-Emitter Voltage ( $I_B = 0$ )	700	V
$V_{EBO}$	Emitter-Base Voltage ( $I_C = 0$ )	5	V
$I_C$	Collector Current	8	A
$I_{CM}$	Collector Peak Current ( $t_p < 5$ ms)	10	A
$I_B$	Base Current	3	A
$I_{BM}$	Base Peak Current ( $t_p < 5$ ms)	6	A
$P_{tot}$	Total Dissipation at $T_c = 25$ °C	52	W
$T_{stg}$	Storage Temperature	-65 to 150	°C
$T_j$	Max. Operating Junction Temperature	150	°C

# BU808DFI

## THERMAL DATA

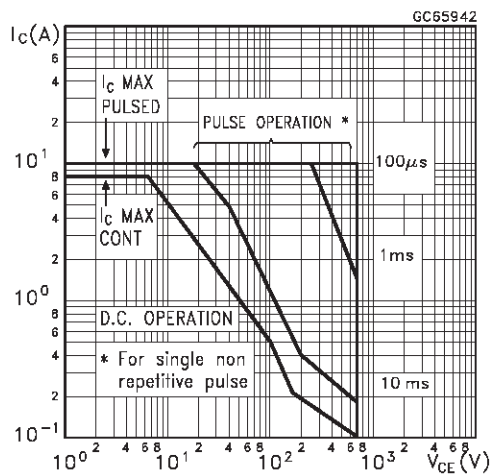
R <sub>thj-case</sub>	Thermal Resistance Junction-case	Max	2.4	°C/W
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## ELECTRICAL CHARACTERISTICS (T<sub>case</sub> = 25 °C unless otherwise specified)

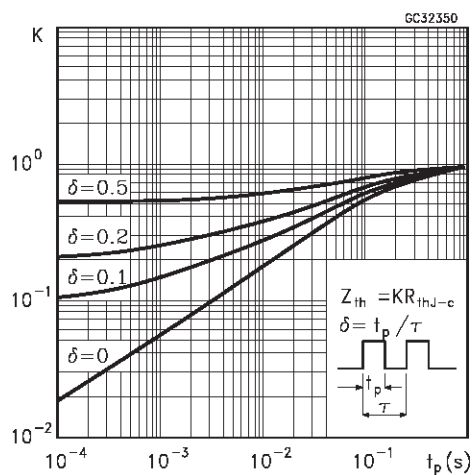
Symbol	Parameter	Test Conditions	Min.	Typ.	Max.	Unit
I <sub>CES</sub>	Collector Cut-off Current (V <sub>BE</sub> = 0)	V <sub>CE</sub> = 1400 V			400	μA
I <sub>CEx</sub>	Collector Cut-off Current (V <sub>BE</sub> = -5V)	V <sub>CE</sub> = 1000 V			400	μA
I <sub>EBO</sub>	Emitter Cut-off Current (I <sub>C</sub> = 0)	V <sub>EB</sub> = 5 V			100	mA
V <sub>CE(sat)*</sub>	Collector-Emitter Saturation Voltage	I <sub>C</sub> = 5 A    I <sub>B</sub> = 0.5 A			1.6	V
V <sub>BE(sat)*</sub>	Base-Emitter Saturation Voltage	I <sub>C</sub> = 5 A    I <sub>B</sub> = 0.5 A			2.1	V
h <sub>FE*</sub>	DC Current Gain	I <sub>C</sub> = 5 A    V <sub>CE</sub> = 5 V I <sub>C</sub> = 5 A    V <sub>CE</sub> = 5 V    T <sub>J</sub> = 100 °C	60 20		270	
t <sub>s</sub> t <sub>f</sub>	INDUCTIVE LOAD Storage Time Fall Time	V <sub>CC</sub> = 150 V    I <sub>C</sub> = 5 A I <sub>B1</sub> = 0.5 A    V <sub>BEoff</sub> = -5 V			3 0.8	μs μs
t <sub>s</sub> t <sub>f</sub>	INDUCTIVE LOAD Storage Time Fall Time	V <sub>CC</sub> = 150 V    I <sub>C</sub> = 5 A I <sub>B1</sub> = 0.5 A    V <sub>BEoff</sub> = -5 V T <sub>J</sub> = 100 °C		2 0.8		μs μs
V <sub>F</sub>	Diode Forward Voltage	I <sub>F</sub> = 5 A			3	V

\* Pulsed: Pulse duration = 300 μs, duty cycle 1.5 %

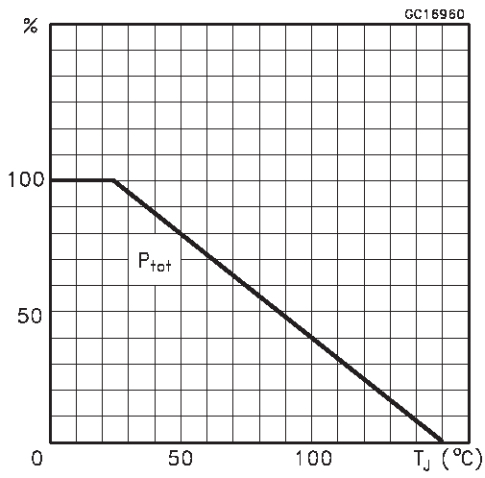
## Safe Operating Area



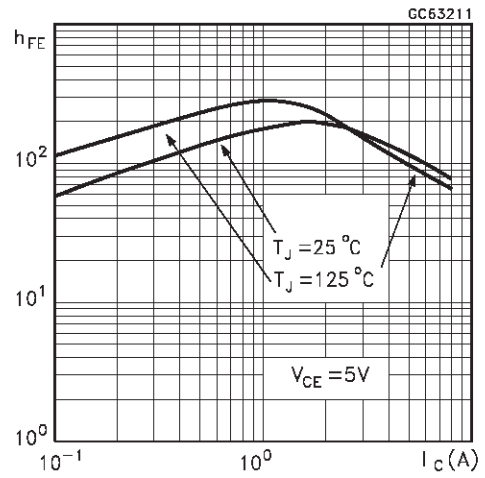
## Thermal Impedance



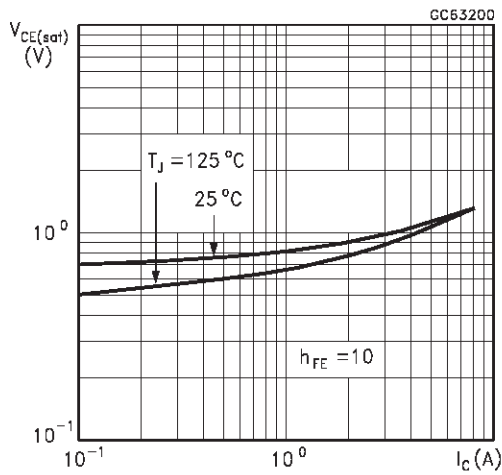
Derating Curve



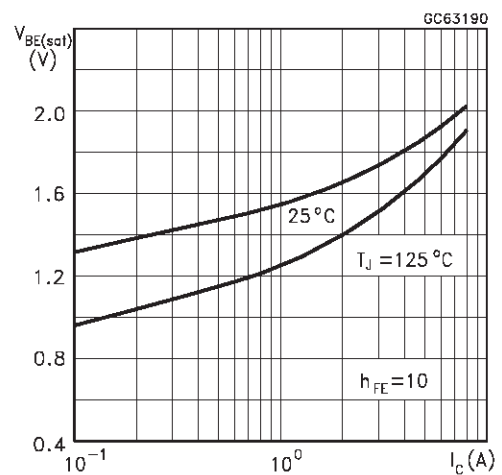
DC Current Gain



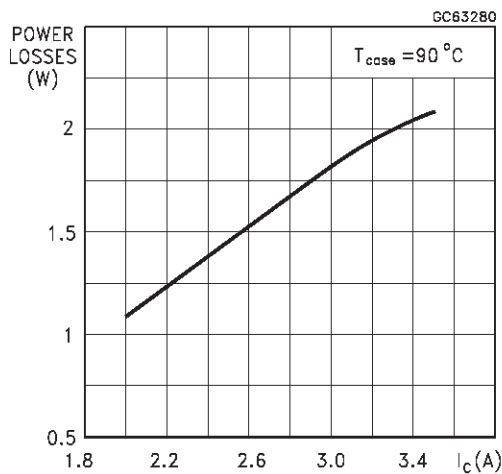
Collector Emitter Saturation Voltage



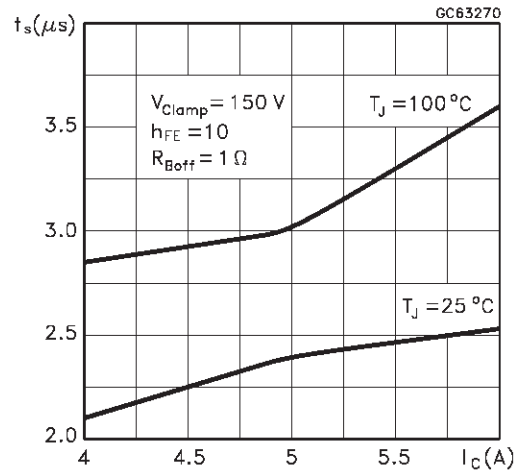
Base Emitter Saturation Voltage



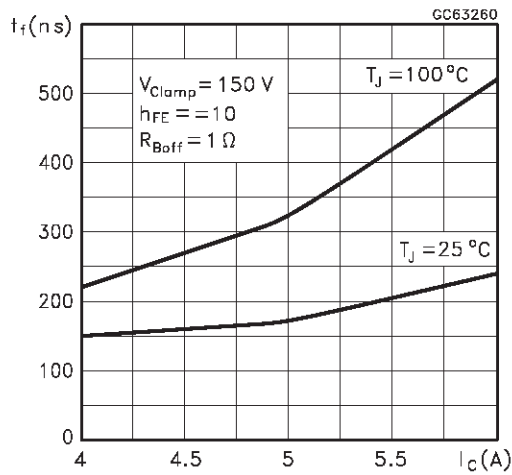
Power Losses at 16 KHz



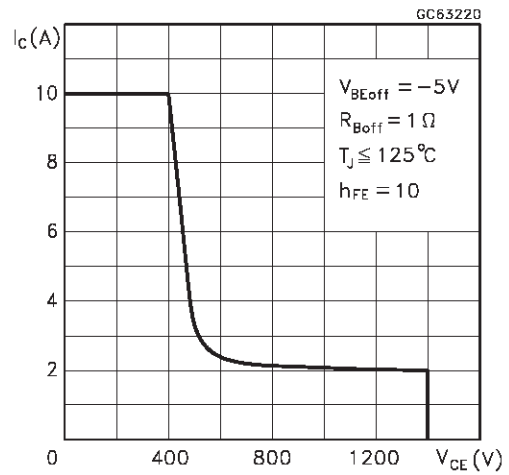
Switching Time Inductive Load at 16KHz



Switching Time Inductive Load at 16KHZ



Reverse Biased SOA



**BASE DRIVE INFORMATION**

In order to saturate the power switch and reduce conduction losses, adequate direct base current  $I_{B1}$  has to be provided for the lowest gain  $h_{FE}$  at  $100\ ^\circ\text{C}$  (line scan phase). On the other hand, negative base current  $I_{B2}$  must be provided to turn off the power transistor (retrace phase).

Most of the dissipation, in the deflection application, occurs at switch-off. Therefore it is essential to determine the value of  $I_{B2}$  which minimizes power losses, fall time  $t_f$  and, consequently,  $T_J$ . A new set of curves have been defined to give total power losses,  $t_s$  and  $t_f$  as a function of  $I_{B2}$  at both 16 KHz scanning frequencies for choosing the optimum negative

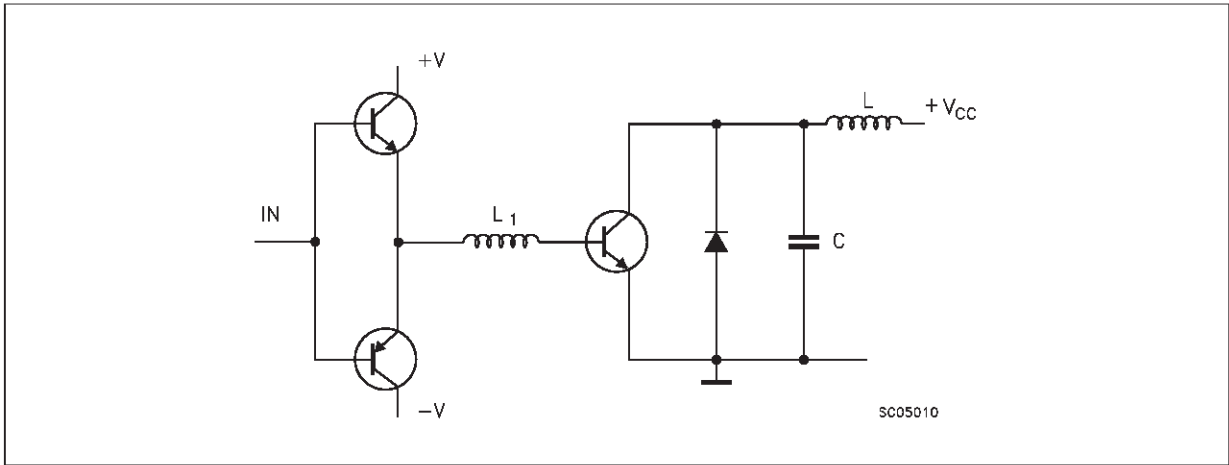
drive. The test circuit is illustrated in figure 1. Inductance  $L_1$  serves to control the slope of the negative base current  $I_{B2}$  to recombine the excess carrier in the collector when base current is still present, this would avoid any tailing phenomenon in the collector current.

The values of  $L$  and  $C$  are calculated from the following equations:

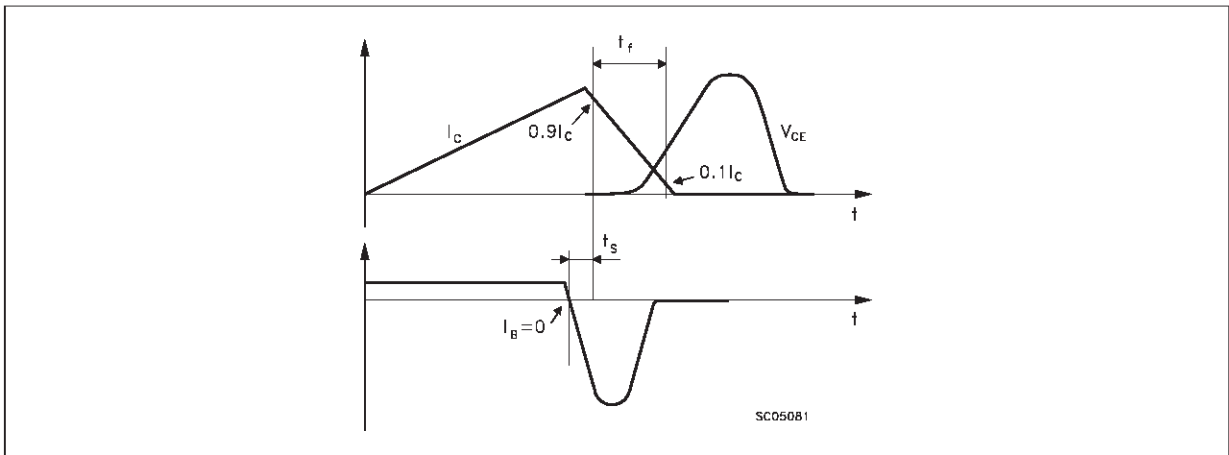
$$\frac{1}{2} L (I_C)^2 = \frac{1}{2} C (V_{CEfly})^2 \quad \omega = 2\pi f = \frac{1}{\sqrt{LC}}$$

Where  $I_C$ = operating collector current,  $V_{CEfly}$ = flyback voltage,  $f$ = frequency of oscillation during retrace.

**Figure 1: Inductive Load Switching Test Circuits.**

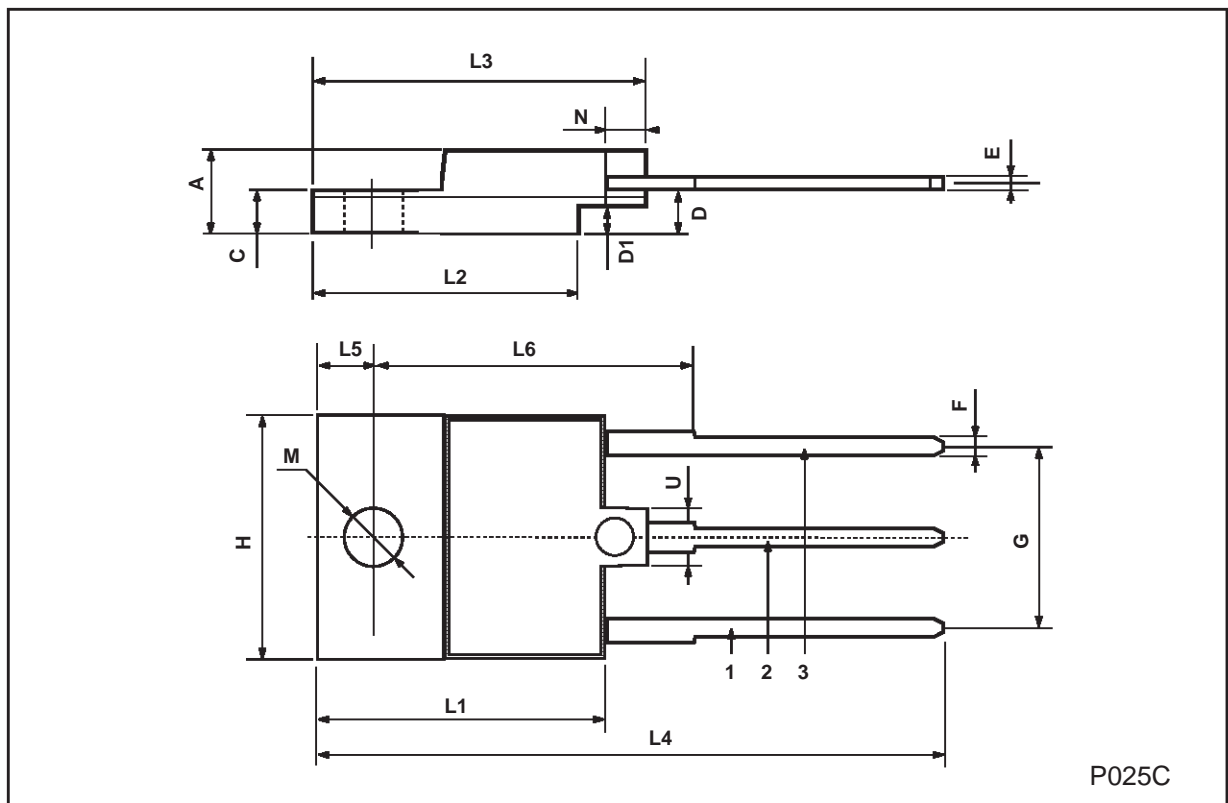


**Figure 2: Switching Waveforms in a Deflection Circuit**



**ISOWATT218 MECHANICAL DATA**

DIM.	mm			inch		
	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.
A	5.35		5.65	0.210		0.222
C	3.3		3.8	0.130		0.149
D	2.9		3.1	0.114		0.122
D1	1.88		2.08	0.074		0.081
E	0.75		1	0.029		0.039
F	1.05		1.25	0.041		0.049
G	10.8		11.2	0.425		0.441
H	15.8		16.2	0.622		0.637
L1	20.8		21.2	0.818		0.834
L2	19.1		19.9	0.752		0.783
L3	22.8		23.6	0.897		0.929
L4	40.5		42.5	1.594		1.673
L5	4.85		5.25	0.190		0.206
L6	20.25		20.75	0.797		0.817
M	3.5		3.7	0.137		0.145
N	2.1		2.3	0.082		0.090
U		4.6			0.181	



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